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## Effect of cell configurations on the performance of citric acid production by a bipolar membrane electro dialysis

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### Abstract

The purpose of this study was to evaluate the effect of cell configurations on the energy consumption and the electroacidification parameters in the production of citric acid using a bipolar membrane electro dialysis (BPED). Three basic cell arrangements, A (anion membrane)–C (cation membrane)–BP (bipolar membrane)–A–C (type I), C–BP–C (type II) and BP–A–C–BP (type III) were discussed and compared. Type I generates acid citrate by acidification with acid sulfate produced from the dissociation of sodium sulfate, and type II produces acid citrate by replacing  $\text{Na}^+$  with  $\text{H}^+$  generated at BPED and type III generates acid citrate by direct splitting sodium citrate. The current density–voltage curves for the three configurations show the typical behaviors given by the coupling of ion transport and electrical field-enhanced water dissociation and are not completely overlapped in the two determined orders due to the change in Donnan potential at the bipolar junction and solution–membrane interface. The magnitudes of cell voltage, current efficiency and energy consumption follow the analogous order as type II < type I < type III, while the potential drop across a bipolar membrane follows the order type II > type I  $\approx$  type III. From the comprehensive considerations of the energy consumption, current efficiency and concentration of the produced acid citrate, it suggests that type II seems to be a favorable cell configuration for the production of citric acid. It is not advisable to manufacture acid citrate by direct splitting its salt. © 2002 Published by Elsevier Science B.V.

*Keywords:* Bipolar membrane; Citric acid; Cell configuration; Water dissociation

### 1. Introduction

Conventionally, most organic acids are produced from fermentation process followed by precipitation and chemical acidification. The product obtained by this technique is usually at low concentration, e.g. 0.2–1N due to the limitation of fermentation process. Because the fermentation process typically operates at near neutral pH; this being maintained via addition of a suitable base. Increasing the product concentration significantly reduces the productivity of the fermentor due to product inhibition. One more disad-

vantages of this method include denaturation of some organic/amino acid on exposure to alkali and acid treatment, high ash content and large discarding of wastes produced from the filtration and precipitation processes.

Bipolar membrane water splitting technology provides an attractive complement to the fermentation technology by removing the product acid, while simultaneously providing an equivalent amount of base for use in adjusting the pH in the fermentor. The fermentor itself can now be operated at relatively low product concentration to assure high productivity. As an added advantage the produced acid is usually at a relatively high concentration so that the subsequent purification via crystallization or other techniques is rel-

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51 atively inexpensive. This technology has been used in  
52 several industries/investigated in experimental set-ups  
53 for producing organic/amino acids [1–4] such as lac-  
54 tic acid [5], citric acid [6], acetate acid [7] as well as  
55 electroacidification of soybean protein [8–10].

56 The principle of the electro-dialytic water-dissocia-  
57 tion process employing a bipolar membrane (BP) is  
58 well documented. If a direct electrical potential (dc) is  
59 established between a bipolar membrane which con-  
60 sists of a layer of an anion exchange membrane and a  
61 layer of a cation exchange membrane, water dissocia-  
62 tion occurs at the interphase and a current is sustained  
63 through the membrane by the migration of hydrogen  
64 and hydroxyl ions to the respective compartments un-  
65 der the fluency of applied dc electric field. By appro-  
66 priately arranging conventional cation-exchange and  
67 anion-exchange membrane on either side of the bipo-  
68 lar membrane, cations and anions of a given organic  
69 salt, e.g. sodium citrate ( $\text{Na}_3\text{Cit}$ ) as discussed here,  
70 could be so directed to meet the  $\text{OH}^-$  and  $\text{H}^+$  in re-  
71 spective compartments to generated separate streams  
72 of alkali and citric acid ( $\text{H}_3\text{Cit}$ ). This new technology  
73 is not only related with the operation conditions but  
74 at large extent, related to the configurations of bipolar  
75 membrane cell stacks as well [4,11,12].

76 Therefore, the main purpose of current research is  
77 to investigate the effect of the cell configurations on  
78  $\text{H}_3\text{Cit}$  production based on water dissociation with  
79 bipolar membranes. We try to correlate the results of  
80 the current density–voltage ( $I$ – $V$ ) curve, current effi-  
81 ciency and energy consumption with the cell configu-  
82 rations.

## 83 2. Experimental

84 The laboratory-scale experimental set-up was com-  
85 posed of one anode and one cathode as well as dif-  
86 ferent number of cation-, anion- and bipolar exchange  
87 membranes inserted between them, forming three dif-  
88 ferent cell configurations as described below.

### 89 2.1. A–C–BP–A–C type (type I)

90 This arrangement is shown in Fig. 1 (a) and con-  
91 sists of a bipolar membrane (BP) operating in con-  
92 junction with two cation exchange membranes (C) and  
93 two anion exchange membranes (A). This is a stan-

94 dard six-compartment stack in conjunction with the  
95 electrodes. The 0.5 M sodium citrate solution is fed  
96 to the acid chamber between the cation side of the  
97 bipolar membrane and the anion membrane and 0.5 M  
98 sodium sulfate solution fed to the other chambers if not  
99 specifically mentioned. This configuration generates  
100 acid citrate in the chamber between the cation side of  
101 bipolar membrane and anion membrane by acidifica-  
102 tion with acid sulfate produced from the dissociation  
103 of sodium sulfate.

### 104 2.2. C–BP–C type (type II)

105 This arrangement is shown in Fig. 1 (b) and con-  
106 sists of a bipolar membrane (BP) operating in con-  
107 junction with two cation exchange membranes (C) to  
108 form a four-compartment stack in combination with  
109 the cathode and anode. The 0.5 M sodium citrate so-  
110 lution is fed to the acid chamber between the cation  
111 side of the bipolar membrane and the cation membrane  
112 neighboring to the cathode and 0.5 M sulfate sodium  
113 solution fed to the other chambers if not specifically  
114 mentioned. The organic salt is converted into organic  
115 acid with the protons produced from the water disso-  
116 ciation transporting into the chamber and the sodium  
117 ions out of the chamber. In this case, acid citrate is  
118 formed by replacing  $\text{Na}^+$  with  $\text{H}^+$  in the chamber be-  
119 tween the cation side of bipolar membrane and cation  
120 membrane.

### 121 2.3. BP–A–C–BP type (type III)

122 This arrangement is shown in Fig. 1 (c) and con-  
123 sists of two bipolar membranes (BP) operating in con-  
124 junction with an anion exchange membrane and a  
125 cation exchange membrane (C) to form an analogous  
126 five-compartment stack in combination with the cath-  
127 ode and anode. The 0.5 M sodium citrate solution is  
128 fed to the chamber between the anion and cation ex-  
129 change membranes and 0.5 M sodium sulfate fed to the  
130 other compartments if not specifically mentioned. This  
131 type generates acid citrate by direct splitting sodium  
132 citrate in the chamber between the cation side of the  
133 bipolar membrane and the anion membrane.

134 Both the ion exchange membranes and bipolar  
135 membranes used here are prepared from our lab.  
136 The cation exchange membrane was prepared by  
137 sulphonating poly(phenylene oxide) (PPO) [13], the

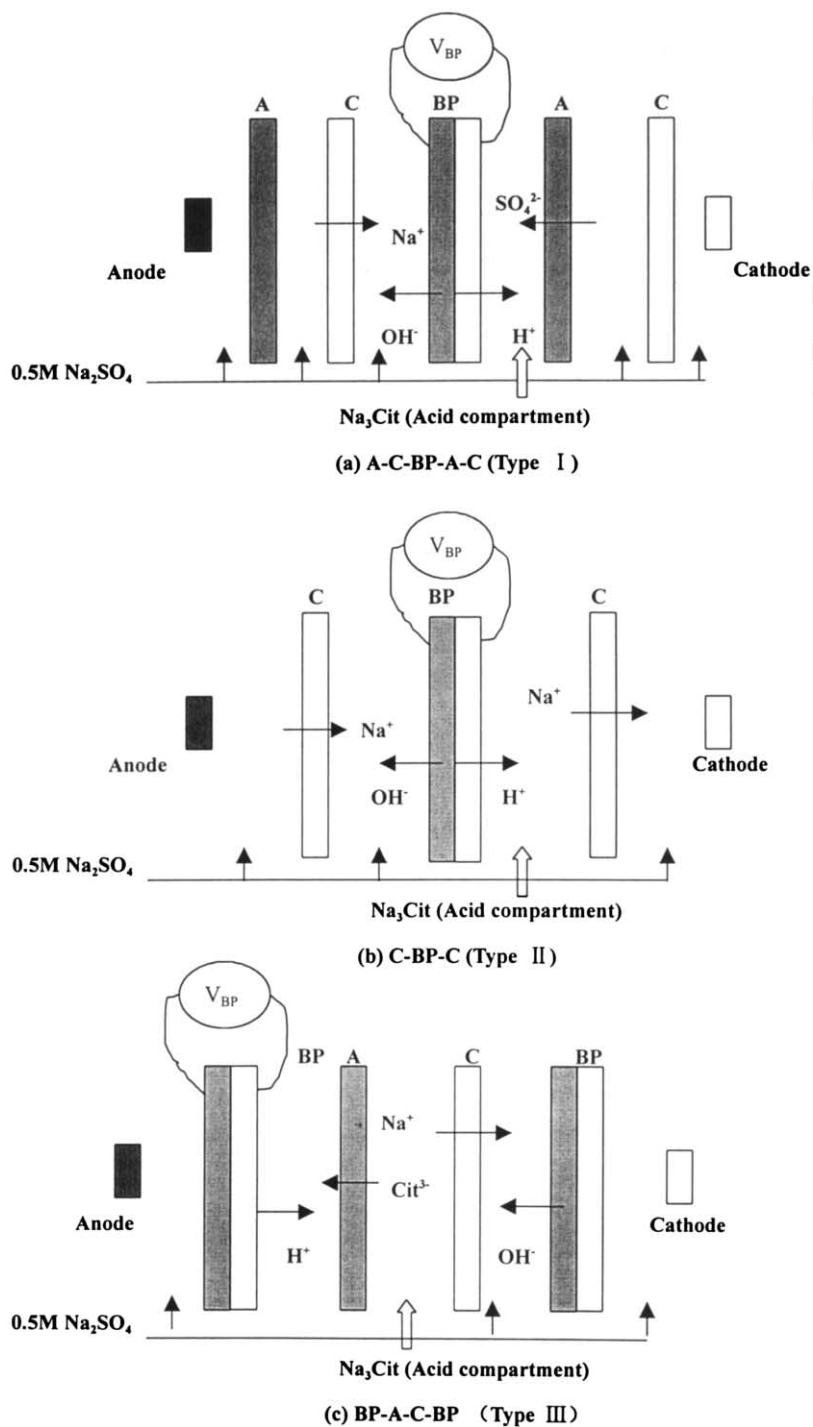


Fig. 1. Scheme of the laboratory cell configurations for citric acid production by electrolytic dialysis (ED) with bipolar membranes.

Table 1  
Characteristics of the electroalytic stack and the membranes

Number of the cell triplets	1
Cationic membrane	Interpolymer type, sulfonic group
Area resistance ( $\Omega \text{ cm}^2$ )	1.6–2.0
Anionic membrane	Interpolymer type, quarternary ammonium group
Area resistance ( $\Omega \text{ cm}^2$ )	2.4–3.0
Bipolar membrane	Composition of the cationic and anionic membranes
Area resistance ( $\Omega \text{ cm}^2$ )	5.0–8.0
Effective membrane area ( $\text{cm}^2$ )	20
Cell thickness (cm)	0.2
Electrodes	Expanded titanium metal net coated with precious metal oxide
Effective volume of solution circulated in each compartment (ml)	500
Flow arrangement	Parallel

138 anion exchange membrane is prepared by brominat-  
139 ing and quarter-aminating PPO [14] and the bipolar  
140 membrane is obtained by casting the cation layer so-  
141 lution onto the anion layer [15]. The salient features  
142 of the stack and the membranes are given in Table 1.

143 The dc potential was established between the end  
144 electrodes of the stack through a CV/CC regulated  
145 power supply (YJ63, Shanghai Huguang Instruments  
146 works). The voltage drop across the stack was directly  
147 read from the indicators on the power supply, while the  
148 potential drop across a bipolar membrane was mea-  
149 sured with a Digital multimeter (model:GDM-8145,  
150 Good will instrument Co. Ltd., Taiwan) through two  
151 platinum probes near to the two surfaces of the lay-  
152 ers. After the electroalytic stack was assembled, the  
153 streams were circulated at a flow rate of 2.5 l/h from  
154 different reservoirs. At a given time, the solution in  
155 acid compartment was sampled and the concentration  
156 of citric acid was determined by titration with standard  
157 sodium hydroxide solution using phenolphthalein as  
158 indicator.

159 The experiments were of batch-type operation. Each  
160 data point was averaged from three independent ex-  
161 perimental runs.

### 162 3. Results and discussions

#### 163 3.1. Current–voltage curves

164 The current–voltage curves were measured under  
165 the condition of 0.5 M sodium citrate in acid cham-  
166 ber and 0.5 M  $\text{Na}_2\text{SO}_4$  in the other chambers for the

167 three cell configurations except that for type I the  
168 curves was also measured under symmetrical concen-  
169 tration of 0.5 M  $\text{Na}_2\text{SO}_4$ . It should be noted that all  
170 the curves were determined in the two orders: one is  
171 from the low current densities to high densities (up-  
172 wards) and the other is from the high densities to  
173 low densities (downwards). The results are depicted  
174 in Figs. 2 and 3. Obviously, the experimental  $I$ – $V$   
175 curves for the three configurations show the typical  
176 behavior given by the coupling of ion transport and  
177 electrical field-enhanced water dissociation [16,17]:  
178 at small voltage, the current is carried mainly by the  
179 salt ions and attains a limiting value. The resistance  
180 of the membrane is more or less increased due to the  
181 migration of salt ions out of the bipolar junction; at  
182 high voltage, most of the current is carried by the  $\text{H}^+$   
183 and  $\text{OH}^-$  ions generated by water dissociation tak-

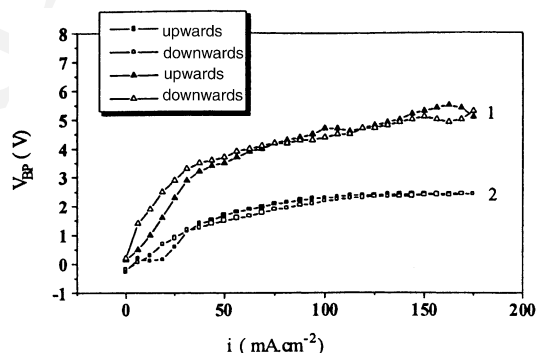


Fig. 2. Experimental  $I$ – $V$  curves for A–C–BP–A–C unit: (1) solu-  
tions in all compartments are 0.5 M  $\text{Na}_2\text{SO}_4$  solution; (2) solution  
in acid compartment is replaced by 0.5 M citric sodium.

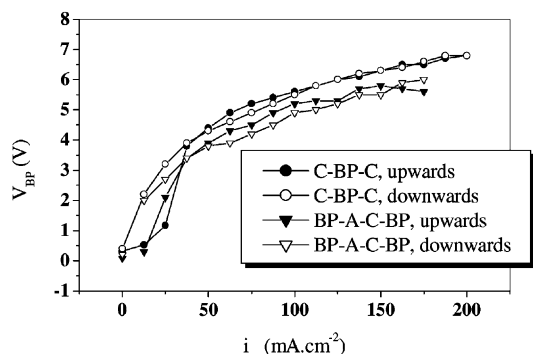


Fig. 3. Experimental  $I$ - $V$  curves for C-BP-C-BP cell units: 0.5 M citric sodium in acid compartment and 0.5 M  $\text{Na}_2\text{SO}_4$  in the other ones.

184 ing place at the bipolar junction, and increases rapidly  
 185 with the voltage. The membrane resistance then be-  
 186 gins to decrease again with the applied voltage. How-  
 187 ever, the magnitudes of voltage values across bipo-  
 188 lar membrane in the considered current density range  
 189 for type I in the different electrolyte are significantly  
 190 different. The voltages measured under symmetrical  
 191 concentration of 0.5 M  $\text{Na}_2\text{SO}_4$  are appreciably larger  
 192 than those obtained in the case of sodium citrate con-  
 193 tained in the acid chamber (Fig. 2). This is mainly due  
 194 to two reasons: one reason is that the conductivity of  
 195 0.5 M sodium sulfate solution ( $2.82 \times 10^4 \mu\text{S}/\text{cm}$ , de-  
 196 termined by DDS 11A conductivity meter, Shanghai  
 197 Leici, China) is higher than that of 0.5 M sodium cit-  
 198 rate solution ( $2.13 \times 10^4 \mu\text{S}/\text{cm}$ ); another one is that  
 199 part of strong electrolyte sodium citrate is transfer to  
 200 weak electrolyte acid citrate due to water dissociation  
 201 during the  $I$ - $V$  measurements. The relative mag-  
 202 nitude of voltages at the case of sodium citrate for dif-  
 203 ferent configurations is not clearly observed and will  
 204 be discussed in the follow at a current density  $I =$   
 205  $100 \text{ mA}/\text{cm}^2$ . In addition,  $I$ - $V$  curves in the two orders  
 206 are not completely overlapped, especially at the case  
 207 of low current densities. This result may be explained  
 208 considering the structures of the bipolar membrane and  
 209 ionic composition changes in the two orders. As men-  
 210 tioned above, the bipolar membrane used in this paper  
 211 is prepared by casting cation membrane solution onto  
 212 an anion membrane and with an asymmetrical layer  
 213 thickness. This membrane structure will easily cause  
 214 a change in Donnan potential at the bipolar junction  
 215 and solution-membrane interface when the ionic com-

position is changed by water dissociation at upwards 216  
 direction before downwards measurements are con- 217  
 ducted and thus caused a change in whole potential 218  
 drop across a bipolar membrane [18]. Nevertheless, 219  
 the Donnan potential is less compared with the ap- 220  
 plied voltage at high current density [19], that is why 221  
 the deviation is less obvious at high current densities 222  
 than that at the low ones. 223

### 3.2. Voltage across the cell stack at a typical current density 224 225

Cell voltage is an important parameter because it is 226  
 related to energy consumption associated with the pro- 227  
 duction of an acid and a base based on bipolar mem- 228  
 branes. The voltage drop, which refers to the varia- 229  
 tion that take place in the ED cell, mainly includes the 230  
 Donnan potential at all solution-membrane interface 231  
 and diffusional potential both in the mono-exchange 232  
 membrane and in the solution as well as the voltage 233  
 across a bipolar membrane. So, it is connected with 234  
 the number of the compartments and the concentra- 235  
 tion of solution in the compartments and thus related 236  
 with cell configurations. Values of the voltage drop for 237  
 the three types of cell arrangement at a typical cur- 238  
 rent density  $I = 100 \text{ mA}/\text{cm}^2$  are plotted in Fig. 4. It 239  
 can be noticed that when a constant current was ap- 240  
 plied (galvanostatic conditions), the cell voltage drops 241  
 keep approximately constant, indicating that the water 242  
 dissociation at this condition approaches to be steady 243  
 state. When the cell voltages are compared within dif- 244  
 ferent cell arrangements, it is interesting to find the 245  
 values increase in the order: type II < type I < type 246

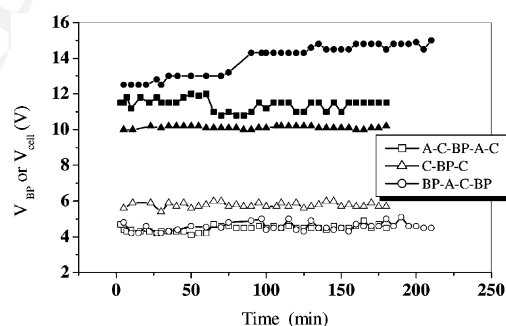


Fig. 4. Time dependence of the voltages across the cell (solid symbols) and BP (open symbols) at  $I = 100 \text{ mA}/\text{cm}^2$  for different cell configurations.

247 III. A difference of the order of  $\sim 4.5$  V was observed  
 248 among the three type of cell configurations. It is not  
 249 difficult to understand the voltage order type II < type  
 250 I because type I has the equal number of bipolar mem-  
 251 brane as the type II but two more mono-membranes  
 252 and chambers as shown in Fig. 1. It is well known that  
 253 the voltage across a bipolar membrane has a relatively  
 254 large contribution to the cell voltage at the state of wa-  
 255 ter dissociation [16,17]. Thus the cell voltage in type  
 256 III has the largest value among the considered config-  
 257 urations because it contains one more bipolar mem-  
 258 brane. When the potentials across the bipolar mem-  
 259 brane for different configurations are compared, the  
 260 values follow the order: type II > type I  $\approx$  type III.  
 261 This is possibly due to the concentration change in  
 262 the adjacent chambers of the bipolar membrane. For  
 263 type I, the electrolyte concentration at both adjacent  
 264 chambers of BP increases due to the production of  $H^-$   
 265 and  $OH^-$  and the migration of  $Na^+$  and  $SO_4^{2-}$  from  
 266 the other chambers. For type III, the situation is anal-  
 267 ogous. But for type II, the electrolyte concentration  
 268 in the chamber between cation side of bipolar mem-  
 269 brane and the cation membrane will not increase with  
 270 the dissociation process, moreover, part of sodium cit-  
 271 rate is transformed into weaker electrolyte citric acid  
 272 ( $pK_1 = 3.13$ ). This is why the voltage across the bipo-  
 273 lar membrane for type II is higher than the other two  
 274 cases. However, this deviation is not so large as the  
 275 difference of cell voltage.

### 276 3.3. Current efficiency

277 The current efficiency  $\eta$  was calculated as [7]

$$278 \eta = \frac{(C_0 - C_t)VF}{NIt} \quad (1)$$

279 where  $C_0$  and  $C_t$  are the equivalent concentration of  
 280 citric acid (acid compartment) at time 0 and  $t$ , respec-  
 281 tively.  $V$  is the circulated volume of solution in each  
 282 compartment,  $I$  the current,  $F$  the Faraday constant and  
 283  $N$  the number of cell triplets.

284 The current efficiency is determined by various time  
 285 intervals from the beginning and therefore it is de-  
 286 pendent of time. As shown in Fig. 5, the current ef-  
 287 ficiency decreases with time which conforms to the  
 288 typical trends, thereby restricting the possibility of ob-  
 289 taining high concentration of acid and alkali [7]. As  
 290 can be seen from Fig. 5, at a given time, the magni-

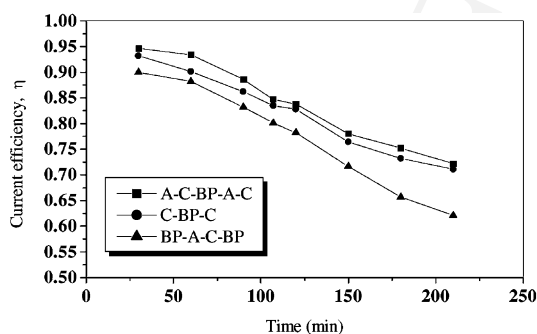


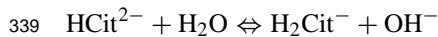
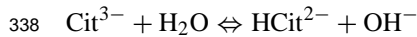
Fig. 5. Current efficiencies for citric acid production vs. time at  $I = 100 \text{ mA/cm}^2$ .

291 tude of current efficiencies for the three cell configu-  
 292 rations follows the order: type III < type II < type  
 293 I. Theoretical interpretation to this order can be based  
 294 on the ionic transport and molecular diffusion in dif-  
 295 ferent cell arrangements.

296 As shown in Fig. 1(a), when a direct current is  
 297 passed between the electrodes in type I cell stack,  
 298 protons produced from cation side of bipolar membrane  
 299 are introduced into the acid compartment and acid-  
 300 ify the organic salt into the corresponding acid at the  
 301 same time. In this process neither other cations com-  
 302 pete with  $H^+$  nor anions with sulfate. So the current  
 303 efficiency is relatively high. For type II, the citric is  
 304 formed in a manner analogous to the above by a direct  
 305 current. In this arrangement, of course, there are some  
 306 possibilities that the produced  $H^+$  ions competitively  
 307 electro-transport and citric acid diffuses through the  
 308 cation membrane to the neighboring compartment to  
 309 that of the acid chamber. However, in this experimen-  
 310 tal conditions, the other cations such as  $Na^+$  ( $0.5 \text{ M}$   
 311  $Na_2SO_4 + 0.5 \text{ M } Na_3Cit = 2.5 \text{ N } Na^+$ ) have a very  
 312 high concentration compared with the  $H^+$  and at the  
 313 same time, the cation membrane has a strong repulsion  
 314 to the coions,  $Cit^{3-}$  ions. Therefore, both the competi-  
 315 tive transport of  $H^+$  ions and the diffusion of citric acid  
 316 seem to be not significant. The large possibility that  
 317 decreases the current efficiency will be caused by the  
 318 neutralization of acid with base transported through  
 319 cation membrane from the cathode compartment un-  
 320 der the electrical field, because cation membrane is  
 321 not completely selective to hydroxyl ions. In addition,  
 322 the concentration of citric acid also tend to be de-  
 323 creased by the water transport from the cathode com-

324 partment to the acid compartment due to the thinner  
 325 of mono-cation membrane and the slight difference of  
 326 the hydrodynamic conditions in these two compart-  
 327 ments. This is supported by the volume change of so-  
 328 lution in the acid and cathode compartments during  
 329 the experiments. So the current efficiency in this type  
 330 is a little lower than that in Type I.

331 In type III, acid citrate is formed by  $H^+$  from BP  
 332 and citrate transported from anion membrane as shown  
 333 in Fig. 1(c). In addition that the unfavorable factors as  
 334 mentioned above decrease the current efficiency, there  
 335 exists a large possibility of competitive diffusion of  
 336  $OH^-$  ions with citrate, which came from the following  
 337 hydrolysis reactions.



340 This competitive diffusion will considerably de-  
 341 crease both the current efficiency and acid concen-  
 342 tration. On the other hand, citrate is larger compared  
 343 with sulfate, its diffusion speed through the mem-  
 344 brane will be lower than sodium or sulfate, which is  
 345 also responsible for the decreased current efficiency.  
 346 This configuration thus tends to achieve a relatively  
 347 low acid concentration, which has been supported by  
 348 the trends in the acid concentration in relation with  
 349 increasing time as presented in Fig. 6.

350 It should be pointed out that citric acid is a weak  
 351 electrolyte experiencing a considerably reduced Don-  
 352 nan exclusion to an anion or cation exchange mem-  
 353 brane, there exists a possibility to be lost by diffusion  
 354 into the neighboring compartment through an anion or

355 cation membrane in all the three types [7]. This dif-  
 356 fused acid also decreases the current efficiency so that  
 357 the experimental current efficiencies are within 95%  
 358 as shown in Fig. 5.

### 359 3.4. Energy consumption

360 The energy consumption  $E$  (kWh/kg) was calcu-  
 361 lated by extrapolating the results for the production of  
 362 1 kg of citric acid based on Eq. (2) [7]

$$363 E = \int \frac{UIdt}{(C_i VM)} \quad (2) \quad 363$$

364 Here,  $U$  is the potential across the cell stack ( $V$ ),  $M$   
 365 is the molar weight of citric acid (192 g/mol). The re-  
 366 sults, shown in Fig. 7, indicate that the energy con-  
 367 sumption follows the order: type II < type I < type  
 368 III which completely conforms to that of cell voltage.  
 369 However, the difference of the energy consumption  
 370 between the types is not proportional to that of cell  
 371 voltage because the energy consumption is determined  
 372 not only by the cell voltage but also by the amount  
 373 of produced organic acid as shown in Eq. (2). Fig. 7  
 374 also shows that the energy difference between differ-  
 375 ent cell configurations increases with an increase in  
 376 the current density.

377 Therefore, both the current efficiency and the en-  
 378 ergy consumption are significantly affected by the cell  
 379 configurations. In this study, we find that type III has  
 380 the highest energy consumption but lowest current ef-  
 381 ficiency, it suggests that manufacture of organic acid is  
 382 not advisable from the direct dissociation of its salts.  
 383 Electroacidification (type I) or ionic replacement (type

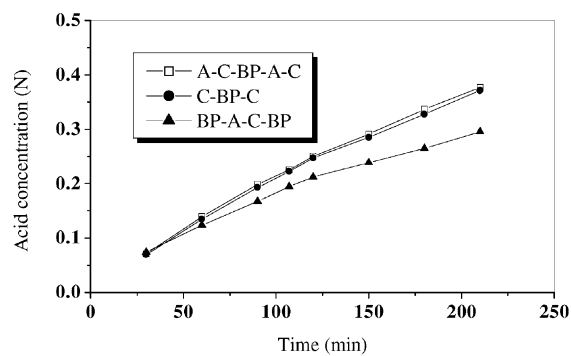


Fig. 6. Time dependence of citric acid concentration in the acid compartment ( $I = 100 \text{ mA/cm}^2$ ).

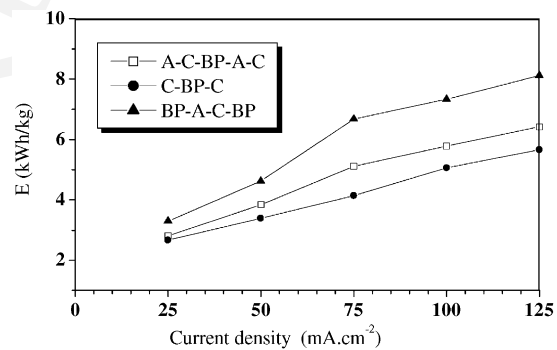


Fig. 7. Energy consumption for the production of citric acid production vs. current density.

II) with BPED is feasible, especially, type II is recommended due to its relatively low energy consumption and simplicity in unit construction though its current efficiency is a little less than that of type II. Nevertheless, better energy consumption values can be obtained by means of a filter type press ED cell in which the compartment thickness and the hydrodynamic conditions are more favorable in order to obtain better current efficiencies at the same time.

It should be noted that calculation of energy consumption is based on the total voltage drop across the stack. It might be lower in the practical use when there are many cell units. The reason is that the voltage drop in the anode and cathode chambers can be neglected when the cell units are many while if there is only one cell unit, the voltage drop across the anode and cathode chamber will cover a little ratio of the total voltage. However, it will not affect the relative magnitude of the investigated configurations because the anode and cathode compartments are same for these configurations.

#### 4. Conclusions

Electrodialysis with bipolar membranes (BPED) provides a convenient way to produce citric acid. In this kind of operation, cell configurations plays an important role on the BPED characteristics.

The current density–voltage curves were measured under the asymmetrical concentration of 0.5 M sodium citrate in the acid chamber and 0.5 M Na<sub>2</sub>SO<sub>4</sub> in the others based on two orders and three fundamental cell arrangements. The curves for the three configurations show the typical behavior given by the coupling of ion transport and electrical field-enhanced water dissociation and are not completely overlapped in the two determined orders due to the change in Donnan potential at the bipolar junction and solution–membrane interface.

The cell voltages, BP potential drop, current efficiency and energy consumption are discussed with the configurations of the cell stacks. The magnitudes of cell voltage follow the order: type II < type I < type III and the potential drop across a bipolar membrane the order: type II > type I ≈ type III. The current efficiency follow the order type II > type I > type III and energy consumption follow the order type I <

type II < type III. From the comprehensive considerations of the energy consumption, current efficiency and concentration of the produced acid citrate, it suggests that type II seems to be a favorable cell configuration for the production of citric acid. It is not advisable to manufacture acid citrate by direct splitting its salt.

It should be mentioned that the above results are obtained with just one production cell between electrode compartments. For a commercial BPED stack with many production cells, the exact values for voltage drop, energy consumption and current efficiency may be changed due to the cell number. However, the relative magnitude of the investigated configurations is expected to be unchanged as long as the basic unit remains the same, because those parameters are seriously affected by ionic transport and molecular diffusion, which are independent of the interior cell number. So, the preliminary results can be act as a basis to investigate a commercial BPED stack with many units for a real citrate fermentation broth, which is scheduled in our lab and will be reported later.

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